

**ISSN 2518-170X (Online),  
ISSN 2224-5278 (Print)**

ҚАЗАҚСТАН РЕСПУБЛИКАСЫ  
ҰЛТТЫҚ ҒЫЛЫМ АКАДЕМИЯСЫНЫҢ

Қ. И. Сәтпаев атындағы Қазақ ұлттық техникалық зерттеу университеті

# Х А Б А Р Л А Р Ы

## ИЗВЕСТИЯ

НАЦИОНАЛЬНОЙ АКАДЕМИИ НАУК  
РЕСПУБЛИКИ КАЗАХСТАН  
Казахский национальный исследовательский  
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## NEWS

OF THE ACADEMY OF SCIENCES  
OF THE REPUBLIC OF KAZAKHSTAN  
Kazakh national research technical university  
named after K. I. Satpayev

SERIES  
OF GEOLOGY AND TECHNICAL SCIENCES

1 (433)

JANUARY – FEBRUARY 2019

THE JOURNAL WAS FOUNDED IN 1940

PUBLISHED 6 TIMES A YEAR

ALMATY, NAS RK

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Қазақстан Республикасы Ұлттық ғылым академиясы "ҚР ҰҒА Хабарлары. Геология және техникалық ғылымдар сериясы" ғылыми журналының Web of Science-тің жаңаланған нұсқасы Emerging Sources Citation Index-те индекстелуге қабылданғанын хабарлайды. Бұл индекстелу барысында Clarivate Analytics компаниясы журналды одан әрі the Science Citation Index Expanded, the Social Sciences Citation Index және the Arts & Humanities Citation Index-ке қабылдау мәселесін қарастыруды. Web of Science зерттеушілер, авторлар, баспашилар мен мекемелерге контент тереңдігі мен сапасын ұсынады. ҚР ҰҒА Хабарлары. Геология және техникалық ғылымдар сериясы Emerging Sources Citation Index-ке енүі біздің қоғамдастық үшін ең өзекті және беделді геология және техникалық ғылымдар бойынша контентке адалдығымызды білдіреді.

НАН РК сообщает, что научный журнал «Известия НАН РК. Серия геологии и технических наук» был принят для индексирования в Emerging Sources Citation Index, обновленной версии Web of Science. Содержание в этом индексировании находится в стадии рассмотрения компанией Clarivate Analytics для дальнейшего принятия журнала в the Science Citation Index Expanded, the Social Sciences Citation Index и the Arts & Humanities Citation Index. Web of Science предлагает качество и глубину контента для исследователей, авторов, издателей и учреждений. Включение Известия НАН РК. Серия геологии и технических наук в Emerging Sources Citation Index демонстрирует нашу приверженность к наиболее актуальному и влиятельному контенту по геологии и техническим наукам для нашего сообщества.

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**ISSN 2518-170X (Online),**

**ISSN 2224-5278 (Print)**

Меншіктенуші: «Қазақстан Республикасының Ұлттық ғылым академиясы» РКБ (Алматы қ.).

Қазақстан республикасының Мәдениет пен ақпарат министрлігінің Ақпарат және мұрагат комитетінде 30.04.2010 ж. берілген №10892-Ж мерзімдік басылым тіркеуіне қойылу туралы куәлік.

Мерзімділігі: жылына 6 рет.

Тиражы: 300 дана.

Редакцияның мекенжайы: 050010, Алматы қ., Шевченко көш., 28, 219 бөл., 220, тел.: 272-13-19, 272-13-18,  
<http://www.geolog-technical.kz/index.php/en/>

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Редакцияның Қазақстан, 050010, Алматы қ., Қабанбай батыра көш., 69а.

мекенжайы: Қ. И. Сәтбаев атындағы геология ғылымдар институты, 334 бөлме. Тел.: 291-59-38.

Типографияның мекенжайы: «Аруна» ЖҚ, Алматы қ., Муратбаева көш., 75.

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**«Известия НАН РК. Серия геологии и технических наук».**

**ISSN 2518-170X (Online),**

**ISSN 2224-5278 (Print)**

Собственник: Республикаинское общественное объединение «Национальная академия наук Республики Казахстан (г. Алматы)

Свидетельство о постановке на учет периодического печатного издания в Комитете информации и архивов Министерства культуры и информации Республики Казахстан №10892-Ж, выданное 30.04.2010 г.

Периодичность: 6 раз в год

Тираж: 300 экземпляров

Адрес редакции: 050010, г. Алматы, ул. Шевченко, 28, ком. 219, 220, тел.: 272-13-19, 272-13-18,  
<http://nauka-nanrk.kz/geology-technical.kz>

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**News of the National Academy of Sciences of the Republic of Kazakhstan. Series of geology and technology sciences.**

**ISSN 2518-170X (Online),**

**ISSN 2224-5278 (Print)**

Owner: RPA "National Academy of Sciences of the Republic of Kazakhstan" (Almaty)

The certificate of registration of a periodic printed publication in the Committee of information and archives of the Ministry of culture and information of the Republic of Kazakhstan N 10892-Ж, issued 30.04.2010

Periodicity: 6 times a year

Circulation: 300 copies

Editorial address: 28, Shevchenko str., of. 219, 220, Almaty, 050010, tel. 272-13-19, 272-13-18,  
<http://nauka-namrk.kz/geology-technical.kz>

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Editorial address: Institute of Geological Sciences named after K.I. Satpayev  
69a, Kabanbai batyr str., of. 334, Almaty, 050010, Kazakhstan, tel.: 291-59-38.

Address of printing house: ST "Aruna", 75, Muratbayev str, Almaty

**N E W S**

OF THE NATIONAL ACADEMY OF SCIENCES OF THE REPUBLIC OF KAZAKHSTAN

**SERIES OF GEOLOGY AND TECHNICAL SCIENCES**

ISSN 2224-5278

Volume 1, Number 433 (2019), 242 – 247

<https://doi.org/10.32014/2019.2518-170X.29>

UDC 539.3 (043.3)

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**PROBLEM ON THE DISTRIBUTION  
OF THE HARMONIC TYPE RELAY WAVE**

**Abstract.** In this paper, we study the class of flat problems on the effect of moving loads on the surface of a laminated plate. The problems of this class are of great practical interest and in addition, can serve as a benchmark for the development of certain numerical algorithms for solving dynamic problems.

Among various periodic and non-periodic motions of deformable medium, plane waves of simple harmonic type, distributed along the surface of a body or half-plane, whose influence is limited by the vicinity of this surface, are of great importance. Therefore, we consider the problem of the distribution of the relay wave.

**Key words:** stratified plates, live-load, waves of Relay, wave equalization.

The equation of motion of a half-plane material in potentials  $\varphi$ ,  $\psi$  is described by wave equations.

$$\begin{aligned} \frac{\partial^2 \varphi}{\partial x^2} + \frac{\partial^2 \varphi}{\partial z^2} &= \frac{1}{a^2} \frac{\partial^2 \varphi}{\partial t^2}; \\ \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial z^2} &= \frac{1}{b^2} \frac{\partial^2 \psi}{\partial t^2}, \end{aligned} \quad (1)$$

where a and b are the distribution speed of the longitudinal and transverse wave, respectively.

We assume that the boundary of the half-plane  $z=0$  is stress-free, i.e.

$$\sigma_{zz} = \sigma_{xz} = 0 \quad (z = 0) \quad (2)$$

Let there be an elastic half-plane  $z \leq 0$ .

Suppose that a flat harmonic wave propagates in the medium, i.e. potentials  $\varphi$  и  $\psi$  will be given in the form of [1]

$$\varphi(x, z, t) = \Phi_0(z) \exp[i(pt - qx)]; \quad \psi(x, z, t) = \Psi_0(z) \exp[i(pt - qx)] \quad (3)$$

$\Phi_0$  and  $\Psi_0$  satisfies the equations

$$\Phi_0'' - \left( q^2 - \frac{p^2}{a^2} \right) \Phi_0 = 0; \quad \Psi_0'' - \left( q^2 - \frac{p^2}{b^2} \right) \Psi_0 = 0. \quad (4)$$

Considering oscillations decaying with depth  $z \rightarrow -\infty$ , there must be met condition

$$q^2 - \frac{p^2}{a^2} > 0; \quad q^2 - \frac{p^2}{b^2} > 0; \quad (5)$$

But since the speeds  $a$  and  $b$  satisfy the inequality  $a > b$ , it suffices to fulfill one condition instead of conditions (5)

$$\frac{p}{q} < b \quad (6)$$

Therefore, solutions of equations (4), decayed at infinity  $z \rightarrow -\infty$ , have the form

$$\Phi_0(z) = A \exp\left(\sqrt{q^2 - \frac{p^2}{a^2}} \cdot z\right); \quad \Psi_0(z) = B \exp\left(\sqrt{q^2 - \frac{p^2}{b^2}} \cdot z\right), \quad (7)$$

and for potentials  $\varphi$  и  $\psi$  we get expressions

$$\varphi = A \exp\left[i(pt - qx) + \sqrt{q^2 - \frac{p^2}{a^2}} z\right]; \quad \psi = B \exp\left[i(pt - qx) + \sqrt{q^2 - \frac{p^2}{b^2}} z\right], \quad (8)$$

where A and B are arbitrary constants of integration.

Putting solutions (7) into the boundary conditions (2), we obtain

$$A\left[2 - \left(\frac{p}{qb}\right)^2\right] + 2iB\sqrt{1 - \left(\frac{p}{qb}\right)^2} = 0; \quad -2iA\sqrt{1 - \left(\frac{p}{qa}\right)^2} + B\left[2 - \left(\frac{p}{qb}\right)^2\right] = 0. \quad (9)$$

In order for the solution of the problem to be non-zero, it is necessary that the determinant of system (9) be non-zero, i.e. to make the relation [2]

$$\left[2 - \left(\frac{p}{qb}\right)^2\right]^2 - 4\sqrt{1 - \left(\frac{p}{qb}\right)^2} \sqrt{1 - \left(\frac{p}{qa}\right)^2} = 0. \quad (10)$$

The ratio  $(p/q)$  is called the propagation velocity of the relay surface wave.

Denoting  $\xi = \left(\frac{p}{qb}\right)^2$  and introducing the Poisson's ratio  $\nu$ , from relation (10) we obtain the equation for the dimensionless velocity of the relay surface wave  $\sqrt{\xi}$ :

$$\xi^3 - 8\xi^2 + 8\xi \frac{2-\nu}{1-\nu} - 8 \frac{1}{1-\nu} = 0. \quad (11)$$

Equation (11) has a single real positive root [1, 3,4].

If through  $z_1$  и  $z_2$  and designate the depth of penetration at which the amplitude of the voltage drops in  $e$  times due to the longitudinal and transverse wave, respectively, then for them we get the expression

$$z_1 = -\frac{l}{2\pi\sqrt{1-a^{-2}b^2\xi}}; \quad z_2 = -\frac{l}{2\pi\sqrt{1-\xi}},$$

at the same time  $l = \frac{1}{q}$  - the wavelength. For example, with  $\nu = 0,5$  we have

$$z_1 = -\frac{l}{2\pi}; \quad z_2 \cong -\frac{l\sqrt{10}}{2\pi}.$$

Let the normal and tangential load intensity  $-F_1(x + Dt)$  и  $-F_2(x + Dt)$  be distributed on the surface  $z = 0$  with constant speed  $D$  i.e. when  $z = 0$  we have boundary conditions

$$\sigma_{zz} = -F_1(x + Dt), \quad \sigma_{xz} = -F_2(x + Dt). \quad (12)$$

Initial conditions for such a problems are absent. [2, 47-50].

We introduce moving coordinates

$$x' = x + Dt; \quad y' = y,$$

and the strokes in the future for simplicity will be omitted. Then for potentials  $\varphi$  and  $\psi$  we get the equations

$$\begin{aligned} \alpha^2 \frac{\partial^2 \varphi}{\partial x^2} - \frac{\partial^2 \varphi}{\partial z^2} &= 0; \\ \beta^2 \frac{\partial^2 \psi}{\partial x^2} - \frac{\partial^2 \psi}{\partial z^2} &= 0; \\ \alpha^2 &= (D/a)^2 - 1; \quad \beta^2 = (D/b)^2 - 1. \end{aligned} \quad (13)$$

General solutions of equations (13) are d'Alembert method and have the form

$$\begin{aligned} \varphi(x, z) &= \varphi_1(x + \alpha z) + \varphi_2(x - \alpha z); \\ \psi(x, z) &= \psi_1(x + \beta z) + \psi_2(x - \beta z). \end{aligned} \quad (14)$$

By virtue of the absence of reflected waves from the lower infinitely distant boundary of the function  $\varphi_2$  and  $\psi_2$  should go to zero and for  $\varphi_1$  and  $\psi_1$  from the boundary conditions (12) we obtain the functional relations [5]

$$\begin{aligned} (\beta^2 - 1)\varphi_1''(x) - 2\beta\psi_1''(x) &= -\frac{F_1(x)}{\rho D^2}(\beta^2 + 1)H(x); \\ 2\alpha\varphi_1''(x) + (\beta^2 - 1)\psi_1''(x) &= -\frac{F_2(x)}{\rho D^2}(\beta^2 + 1)H(x). \end{aligned} \quad (15)$$

From relations (15) we get

$$\begin{aligned} \varphi_1''(x) &= \frac{\beta^2 + 1}{\rho D^2} [(\beta^2 - 1)F_1(x) + 2\beta F_2(x)]H(x)\Delta^{-1}; \\ \psi_1''(x) &= \frac{\beta^2 + 1}{\rho D^2} [2\alpha F_1(x) - (\beta^2 - 1)F_2(x)]H(x)\Delta^{-1}; \\ \Delta &= 4\alpha\beta + (\beta^2 - 1)^2. \end{aligned} \quad (16)$$

Using dependencies (16) for stress values, we obtain the expression

$$\begin{aligned}
\Delta \cdot \sigma_{xx} &= -(\beta^2 - 2\alpha^2 + 1)[(\beta^2 - 1)F_1(x + \alpha z) + 2\beta F_2(x + \alpha z)] \times \\
&\times H(x + \alpha z) + 2\beta[2\alpha F_1(x + \beta z) - (\beta^2 - 1)F_2(x + \beta z)]H(x + \beta z); \\
\Delta \cdot \sigma_{zz} &= -(\beta^2 - 1)[(\beta^2 - 1)F_1(x + \alpha z) + 2\beta F_2(x + \alpha z)]H(x + \alpha z) - \\
&- 2\beta[2\alpha F_1(x + \beta z) - (\beta^2 - 1)F_2(x + \beta z)]H(x + \beta z); \\
\Delta \cdot \sigma_{xz} &= -2\alpha[(\beta^2 - 1)F_1(x + \alpha z) + 2\beta F_2(x + \alpha z)]H(x + \alpha z) + \\
&+ (\beta^2 - 1)[2\alpha F_1(x + \beta z) - (\beta^2 - 1)F_2(x + \beta z)]H(x + \beta z); 
\end{aligned} \tag{17}$$

$$H(\varsigma) = \begin{cases} 1, & \varsigma \geq 0 \\ 0, & \varsigma < 0 \end{cases},$$

and for shift  $u$  and  $w$  accordingly

$$\begin{aligned}
u &= -\frac{\beta^2 + 1}{\rho D^2 \Delta} [(\beta^2 - 1)F_3(x + \alpha z) + 2\beta F_4(x + \alpha z)]H(x + \alpha z) + \\
&+ \beta \frac{\beta^2 + 1}{\rho D^2 \Delta} [2\alpha F_3(x + \beta z) - (\beta^2 - 1)F_4(x + \beta z)]H(x + \beta z), \\
w &= -\alpha \frac{\beta^2 + 1}{\rho D^2 \Delta} [(\beta^2 - 1)F_3(x + \alpha z) + 2\beta F_4(x + \alpha z)] \times \\
&\times H(x + \alpha z) - \frac{\beta^2 + 1}{\rho D^2 \Delta} [2\alpha F_3(x + \beta z) - (\beta^2 - 1)F_4(x + \beta z)]H(x + \beta z)
\end{aligned} \tag{18}$$

where  $F_3(x) = \int_0^x F_1(\xi) d\xi$ ;  $F_4(x) = \int_0^x F_2(\xi) d\xi$ .

Let it be  $F_2 = 0$  and consider the stress  $\sigma_{xx}$  on the boundary  $z = 0$ . We obtain

$$\sigma_{xx} = F(v, D_0)F_1(x); \quad D_0 = D/a,$$

$$\text{where } F(v, D_0) = \frac{A_1(v, D_0) - A_2(v, D_0)B(v, D_0)}{A_1(v, D_0) - A_2(v, D_0)},$$

$$A_1 = (1 - 2v)^{3/2} \sqrt{(D_0^2 - 1)(1 - v) - (1 - 2v)};$$

$$A_2 = [D_0^2(1 - v) - (1 - 2v)]$$

$$B = [D_0^2(1 - v) - (D_0^2 - 1)(1 - 2v)]$$

Let an elastic layer  $0 \leq z > -h$   $|x| < \infty$  lie on the half-space  $z \leq -h$ , over the surface of which the normal load is distributed, i.e. when  $z = 0$  we have boundary conditions

$$\sigma_{zz}^{(0)} = -F(x + Dt); \quad \sigma_{xz}^{(0)} = 0. \tag{19}$$

The sizes and parameters of the layer will be denoted by the index "0", and the half-space - by the index "1".

At the contact boundary  $z = -h$ , you can set the conditions: hard contact

$$\sigma_{zz}^{(0)} = \sigma_{zz}^{(1)}; \quad \sigma_{xz}^{(0)} = \sigma_{xz}^{(1)}; \quad u_0 = u_1; \quad w_0 = w_1; \quad (20)$$

perfect contact

$$\sigma_{zz}^{(0)} = \sigma_{zz}^{(1)}; \quad \sigma_{xz}^{(0)} = \sigma_{xz}^{(1)} = 0; \quad w_0 = w_1; \quad (21)$$

Can be set other conditions for  $z = -h$ .

In moving coordinates, solutions of equations for potentials in a layer and a half-plane have the form [3, 171-176].

$$\begin{aligned} \alpha_j^2 \frac{\partial^2 \varphi_j}{\partial x^2} - \frac{\partial^2 \varphi_j}{\partial z^2} &= 0; \quad \beta_j^2 \frac{\partial^2 \psi_j}{\partial x^2} - \frac{\partial^2 \psi_j}{\partial z^2} = 0; \\ \left( x' = \frac{x + Dt}{h}; \quad y' = \frac{y}{h}; \quad \varphi_0 = \frac{\varphi_0}{h^2}; \quad \psi_0 = \frac{\psi_0}{h^2} \right) \end{aligned} \quad (22)$$

Putting (22) into the boundary conditions (20), we obtain a system of functional equations which using in expressions for displacements  $u_j, w_j$  and stresses  $\sigma_{ij}$ , we obtain the solution of the problem.

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## ГАРМОНИКАЛЫҚ ТИПТЕГІ РЕЛЕЙ ТОЛҚЫНДАРЫНЫҢ ТАРАЛУЫ ЖАЙЛЫ ЕСЕП

**Аннотация.** Жұмыста қатпарлы пластинкалардың бетіне қозғалмалы жүктемелердің әсері туралы бірнеше жазық есептер класы зеріттеді. Осы типтес динамикалық есептер проблемалары жайлы смәселелерді шешүгө арналған белгілі сандық алгоритмдерді дамытудың негізгі бағыты бола алымен қызығушылық тудырады. Деформацияланатын ортаның әртурлі периодты және преиодтты емес қозғалыстарының арасында шектелген дененің бетіне немесе жарты жазықтыққа тарайтын қарапайым гармоникалық үлгідегі жазық толқындар әсер етеді. Соңдықтан да Релей толқынының таралуын зерттейтін боламыз.

**Түйін сөздер:** қатпарлы пластинкалар, қозғалмалы жүктеме, Релей толқындары, толқындар тендеуі.

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## ЗАДАЧА О РАСПРОСТРАНЕНИИ ВОЛНЫ РЕЛЕЯ ГАРМОНИЧЕСКОГО ТИПА

**Аннотация.** В работе исследуем класс плоских задач о воздействии подвижных нагрузок на поверхность слоистой пластиинки. Задачи данного класса представляют большой прикладной интерес и, кроме того, могут служить эталоном для разработки тех или иных численных алгоритмов для решения динамических задач. Среди различных периодических и непериодических движений деформируемых сред важное значение имеют плоские волны простого гармонического типа, распространяющиеся по поверхности тела или полу-плоскости, влияние которых ограничивается окрестностью этой поверхности. Поэтому рассмотрим задачу о распространении волн Релея.

**Ключевые слова:** слоистые пластиинки, подвижная нагрузка, волны Релея, волновые уравнение.

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**ISSN 2518-170X (Online), ISSN 2224-5278 (Print)**

<http://www.geolog-technical.kz/index.php/en/>

Верстка Д. Н. Калкабековой

Подписано в печать 06.02.2019.  
Формат 70x881/8. Бумага офсетная. Печать – ризограф.  
16,7 п.л. Тираж 300. Заказ 1.

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