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ҰЛТТЫҚ ФЫЛЫМ АКАДЕМИЯСЫ

Satbayev University

# **ХАБАРЛАРЫ**

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## **ИЗВЕСТИЯ**

НАЦИОНАЛЬНОЙ АКАДЕМИИ  
НАУК РЕСПУБЛИКИ  
КАЗАХСТАН  
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## **NEWS**

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*NAS RK is pleased to announce that News of NAS RK. Series of geology and technical sciences scientific journal has been accepted for indexing in the Emerging Sources Citation Index, a new edition of Web of Science. Content in this index is under consideration by Clarivate Analytics to be accepted in the Science Citation Index Expanded, the Social Sciences Citation Index, and the Arts & Humanities Citation Index. The quality and depth of content Web of Science offers to researchers, authors, publishers, and institutions sets it apart from other research databases. The inclusion of News of NAS RK. Series of geology and technical sciences in the Emerging Sources Citation Index demonstrates our dedication to providing the most relevant and influential content of geology and engineering sciences to our community.*

Қазақстан Республикасы Үлттық гылым ақадемиясы «ҚР ҰҒА Хабарлары. Геология және техникалық гылымдар сериясы» гылыми журналының Web of Science-тің жаңаланған нұсқасы Emerging Sources Citation Index-те индекстелуге қабылданғанын хабарлайды. Бұл индекстелу барысында Clarivate Analytics компаниясы журналды одан әрi the Science Citation Index Expanded, the Social Sciences Citation Index және the Arts & Humanities Citation Index-ке қабылдау мәселесін қарастыруды. Web of Science зерттеушілер, авторлар, баспашилар мен мекемелерге контент тереңдігі мен сапасын ұсынады. ҚР ҰҒА Хабарлары. Геология және техникалық гылымдар сериясы Emerging Sources Citation Index-ке енүі біздің қоғамдастық үшін ең өзекті және беделді геология және техникалық гылымдар бойынша контентке адалдығымызды білдіреді.

НАН РК сообщает, что научный журнал «Известия НАН РК. Серия геологии и технических наук» был принят для индексирования в Emerging Sources Citation Index, обновленной версии Web of Science. Содержание в этом индексировании находится в стадии рассмотрения компанией Clarivate Analytics для дальнейшего принятия журнала в the Science Citation Index Expanded, the Social Sciences Citation Index и the Arts & Humanities Citation Index. Web of Science предлагает качество и глубину контента для исследователей, авторов, издавателей и учреждений. Включение Известия НАН РК. Серия геологии и технических наук в Emerging Sources Citation Index демонстрирует нашу приверженность к наиболее актуальному и влиятельному контенту по геологии и техническим наукам для нашего сообщества.

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## **THE RESEARCH OF CIRCULAR SAW BLADE STABILITY STATE FOR THERMAL FRICTIONAL CUTTING BY THE METHOD OF CALCULATION IN THE FORM OF A HINGELESS CIRCULAR ARCH**

**Abstract.** The productive and uninterrupted operation of the chemical, oil, geological exploration and other sectors of the national economy of the Republic of Kazakhstan directly depends on the quality of manufacturing of parts and components of process equipment. The manufacture, repair and restoration of parts and assemblies of technological equipment are carried out by mechanical repair production, where the main mechanical operation is the cutting operation. The authors have developed a method for thermal friction cutting with pulsed cooling. A disc saw is used as a cutting tool.

In this article, a scientific and theoretical study of the state of stability of a disc saw for thermal friction cutting was carried out by the calculation method in the form of a circular hingeless arch.

A calculation method is proposed for determining the state of stability of a saw blade. The form of buckling of a hingeless arch is also determined. Based on the results of the research, the following conclusions can be drawn: the effectiveness of the finite difference method for calculating the state of stability of a circular saw is shown, using a rod calculation model in the form of a circular hingeless arch for half of the circular saw that has penetrated into the body of the material being cut, the form of buckling under a complex loading scheme has a “multi-wave” character.

**Key words.** Circular saw blade, rod model, thermal frictional cutting, bending moments, cross forces, longitudinal forces, hingeless arch stability.

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## **ТЕРМОФРИКЦИОНДЫ КЕСУГЕ АРНАЛҒАН ДОМАЛАҚ ШАРНИРСІЗ АРКА ТҮРІНДЕ ЕСЕПТЕУ ӘДІСІМЕН ДИСКІЛІ АРАНЫң ОРНЫҚТЫЛЫҚ ЖАҒДАЙЫН ЗЕРТТЕУ**

**Аннотация.** Қазақстан Республикасының химия, мұнай, геологиялық барлау және басқа да халық шаруашылығы салаларының өндірістік және үздіксіз жұмысы технологиялық жабдықтың тетіктері мен тораптарын даярлау сапасына тікелей тәуелді болады. Технологиялық жабдықтардың тетіктері мен тораптарын даярлау, жөндеу және қайта қалпына келтіру жұмыстарымен механикалық-жөндеу өндірісі айналысады және ондағы орындалатын негізгі механикалық операциялардың бірі – кесу операциясы. Авторлар тарапынан термофрикциондық кесу тәсілі жасалған. Кесуші құрал ретінде бұл тәсілде дискілі аралар қолданылады. Әр түрлі металл материалдарды термофрикциондық кесу үшін айналмалы дискілі аралардың жұмыс істеу барысында, оларда күштік және инерциялық әсерлерден туындаған құрделі кернеулі-деформацияланған құбылыстар пайда болады, осындағы мәселені шешу қабылданған есептеу моделіне тәуелді болады. Бұл мақалада термофрикциондық кесу үшін дискілі араның тұрақтылығының күйін домалак шарнирсіз арка түрінде есептеу әдісімен ғылыми-теориялық зерттеу жүргізілді. Кесілеттің материалдың денесіне батыра кірген дискілі араның жартысына арналған дөңгелек шарнирсіз арка түріндегі стерженді модельді қолдануға негізделген дискілі араның орнықтылығының жағдайын анықтау әдістемесі ұсынылады. Шарнирсіз дөңгелек арканың, июші моменттердің эпюрінің, сондай-ақ көлденен және бойлық күштердің эпюрінің есептік схемасы келтіріледі. Сондай-ақ, шарнирсіз арканың орнықтылығын жоғалту пішіні анықталды. Зерттеу

нәтижесі бойынша қорытынды: кесілетін материалға енетін дискілі араның жартысына арналған дөңгелек шарнирсіз арка түрінде есептеудің өзекті моделін пайдалана отырып, дискілі араның орнықтылығының жағдайын есептеу үшін соңғы айырмашылықтар әдісін қолдану тиімділігі көрсетілген, жүктеудің күрделі сұлбасында орнықтылықты жоғалту пішіні «көп толқындылық» сипатқа ие болады.

**Түйін сөздер:** дискілі ара, стержді модель, термофрикционды кесу, иілу моменті, көлденең күштер, бойлық күштер, шарнирсіз арканың тұрақтылығы.

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## **ИССЛЕДОВАНИЕ СОСТОЯНИЯ УСТОЙЧИВОСТИ ДИСКОВОЙ ПИЛЫ ДЛЯ ТЕРМОФРИКЦИОННОЙ РЕЗКИ МЕТОДОМ РАСЧЕТА В ВИДЕ КРУГОВОЙ БЕСШАРНИРНОЙ АРКИ**

**Аннотация.** Производительная и бесперебойная работа химической, нефтяной, геологоразведочной и других отраслей народного хозяйства Республики Казахстан напрямую зависят от качества изготовления деталей и узлов технологического оборудования. Изготовлением, ремонтом и восстановлением деталей и узлов технологического оборудования занимается ремонтно-механическое производство, где основной механической операцией является отрезная операция. Авторами разработан способ термофрикционной отрезки с импульсным охлаждением. В качестве режущего инструмента применяется дисковая пила. В процессе работы вращающихся дисковых пил для термофрикционной отрезки различных металлических материалов в них возникают сложные напряженно-деформированные явления, вызванные силовыми и инерционными воздействиями, решение подобной задачи зависит от принятой расчетной модели. В данной статье выполнено научно-теоретическое исследования состояния устойчивости дисковой пилы для термофрикционной резки

методом расчета в виде круговой бесшарнирной арки. Предлагается методика расчета определения состояния устойчивости дисковой пилы, которая основана применению стержневой модели в виде круговой бесшарнирной арки для половины дисковой пилы, проникшей в тело разрезаемого материала. Приводятся расчетная схема бесшарнирной круговой арки, эпюра изгибающих моментов, а также эпюра поперечных и продольных сил. Также определена форма потери устойчивости бесшарнирной арки. По результатам исследований можно сделать следующие выводы: показана эффективность применения метода конечных разностей для расчета состояния устойчивости дисковой пилы, используя стержневого моделья расчета в виде круговой бесшарнирной арки для половины дисковой пилы проникшей в тело разрезаемого материала, форма потери устойчивости при сложной схеме загружения имеет «многоволновой» характер.

**Ключевые слова:** дисковая пила, стержневый модель, термофрикционная резка, изгибающий момент, поперечные силы, продольные силы, устойчивость бесшарнирной арки.

**Introduction.** Traditional thermal frictional processing technology based on the softening of the processed material in the cutting zone on account of the high rate of sliding friction. At the same time, the higher the velocity, the more the amount of heat accumulated in the contact. Consequently, the processed material is subjected to a greater softening and the cutting circular saw blade retains strength properties due to the particular part location minimizations periphery of the disk in contact. However, an excessive increase in velocity leads to a tightening of requirements for equipment. So, the average cost of the machine by increasing the speed  $V = 30 \text{ m/s}$  to  $V > 70 \text{ m/s}$ , increases 5÷7 times and increases the power consumption (for machines equipped with engines thermal frictional processing 22-40 kW). Persistence of the circular saw blade in the range  $V = 35 \div 70 \text{ m/s}$  is low, as it does not have time to cool down. The authors have developed resource saving technology of thermal frictional processing implemented at low speeds (Sherov, et all, 2017 a: 10, Nasad, et all, 2019: 7, Khodzhibergenov, et all, 2015: 3, Dudak, et all, 2017: 8), one of which is thermal frictional cutting with the localization of the thermal field due to a pulsed cooling (Sherov, et all, 2020 b: 4, Kadyrov, et all, 2021: 9, Balgabekov, et all, 2014: 3). Figure 1 shows photographs of circular saw blades of various designs.



Figure 1. Photo of circular saw blades of various designs

When thermal frictional cutting with pulsed cooling one of the indicators of the quality of the cut is perpendicular. Providing of perpendicularity of cut depends largely on the stability of the circular saw blade. In this regard, the study circular saw blade stability of the state by calculating in the form of hingeless circular arch is an urgent task.

Research materials and methods. In operation, the process of the rotating circular saw blades for thermal frictional cutting of various metallic materials complex stressedly-deformed facts caused by the inertial force and the inertional impacts. There is a solution that depends on the accepted calculated model (rod, plate, etc.)

In this research to calculate the cutting saws were accepted the rod model in the form of a hingeless circular arch for half of the circular saw blade, piercing into the body of the material being cut.

**Results.** Figure 2 shows the calculated scheme of a hingeless circular arch. All external loads arising in the process of cutting (radial and tangential) are put to a single value of  $q$ .

The geometry of the arch axis (see. Figure 2)

$x_i$  - abscissa current i-th section;

$y_i$  - the same, the ordinate;

$\phi_i$  - angle of the tilt tangent to the x-axis held in i-th section.

For arches, the axis of which is delineated by a circle is taken:

$$y_i = \sqrt{R^2 - \left(\frac{l}{2} - x_i\right)^2} - R + f \quad (1)$$

$$R = \frac{f}{2} + \frac{l^2}{8f} = l/2 - \text{The radius of the circle} \quad (2)$$

$$\sin \phi_i = (l - 2x_i)/2R; \quad \cos \phi_i = (y_i + R - f)/R \quad (3)$$

u - axis parallel to the tangent; v - axis normal to the tangent; s - size of the bow arch.

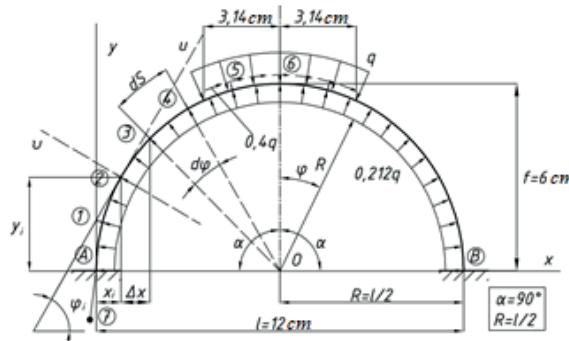


Figure 2. The calculated scheme of a hingeless circular arch

The differential equation of the bent axis of a circular bar of small curvature has the form (through the bending moment) (Darkov, et all, 2010 a: 656; Smirnov, et all, 1981: 512; Burgakov, et all, 1983: 255; Klein, et all, 1980: 384; Rabinovich, 1960: 516):

$$\frac{d^2u}{ds^2} + \frac{u}{\rho^2} = -\frac{M}{EJ} \text{ or } \frac{d^2u}{d\phi^2} + u = -\frac{M\rho^2}{EJ} \quad (4)$$

where (see Figure 2):  $ds$  - the length of the elementary arc arch axis;  $\phi$  - angle counted relatively to the center of vertical axis of the circle;  $d\phi$  - elementary opening angle;  $M$  - a function of the bending moment in the cross sections on the axis of the arch;  $EJ$  - bending stiffness of the arch axis;  $u$  -  $v$  linear movement along the axis;  $d_u$  - elementary movement ( $\rho = R$ ) - for circular arch.

For hingeless arch when effects to loads indicated in Figure 2 (three times statically indeterminate system) the classical method of forces (by the method of elastic center) was made static analysis (Darkov, 2008 b:420; Imanbaeva, et all, 2011: 158; Lukashevich, 2003: 135; Doihen, et all, 2001: 203), and received the diagrams of internal forces  $M$ ,  $Q$ ,  $N$ .

Figure 3 shows the bending moment diagram.

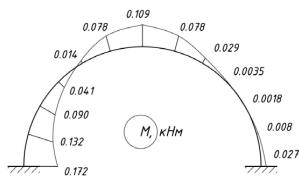


Figure 3. The diagram of bending moments

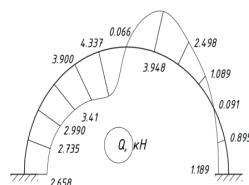


Figure 4. The diagram of cross forces

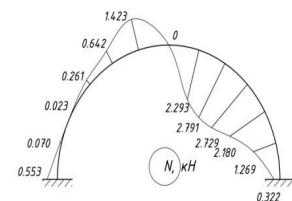


Figure 5. The diagram of the longitudinal forces

The ordinate values of bending moment diagram  $M$  can be inserted into equation (4).

To make equation (4) we use the method of finite differences using a curved grid (Iljin, 1990: 268; Filippova, et all, 2016: 162; Zenkevich, et all, 1974: 239; Aleksandrov, et all, 1990 a: 400). We transform the equation (4) of the intensity of the external load of  $q$ , the critical values which, in the future, we seek out when we solve the problem of stability of the curved bar (Klein, 1980: 384; Aleksandrov, et all, 2000 b: 560; George, et all, 1984: 333; Togizbayeva, et all, 2020: 9; Zhunusbekova, et all, 2016: 4).

We allow the following symbols:

$$K^2 = \frac{\alpha \cdot q \cdot R^2}{EJ} + 1. \quad (5)$$

$K^2$  - parameter of the external load.

We can determine the value of the critical load intensity with the known value of «K»:

$$q_{kp} = \frac{EJ(K^2 \cdot 1)}{R^2}. \quad (6)$$

The original differential equation (5), expressed in load «q» will take this view after the transformation as follows:

$$\frac{d^4u}{d\phi^4} + \frac{d^2u}{\phi^2} = \frac{q}{EJ_{min}} \text{ or } \frac{d^4u}{ds^4} + \frac{1}{R^2} \cdot \frac{d^2u}{ds^2} = \frac{q}{EJ_{min}} \quad (7)$$

We can write the equation (7) in finite differences through radial grid parameters  $u$ ,  $\phi_0$ . Taking into account the symmetry we divide the half-arches (see Figure 2) into 6 equal parts with the parameters:  $R = 6 \text{ cm}$ ;  $d\phi = 90^\circ/6 = 15^\circ = 0.2618$ ;  $dS = Rd\phi = 0,01571 \text{ (m)}$ .

Figure 2, the unit “A” - the outlined unit, “7” - contoured unit. We exclude their value of movement, using the boundary conditions in the “A” unit:

$U_A = 0$  (fixed “heel” arches).

$(du/dx)_A = 0$ ;  $(U_7 - U_1)/\phi_1 = 0$ ;  $(\phi_1 = dx = 15^\circ)$ , hence:

$$U_7 = U_1, \text{ t.e. } U_A = 0; U_7 = U_1; dS \approx \Delta S = 0,01571 \text{ m.} \quad (8)$$

For the i-th unit of the radial grid (See Figure 5), equation (6) in finite differences will be:

$$\frac{1}{(\Delta S)^4} [(u_s + u_t) - 4(u_k + u_l) + 6u_o] + \left[ \frac{1}{R^2} \cdot \frac{1}{(\Delta S)^2} (u_k + u_l - 2u_o) \right] = k^2(\alpha) \quad (9)$$

( $\alpha = q/q_0$  conditional coefficient of load  $q$  (see Figure 1), ( $q_0$  - conditionally accepted value).

The number of calculated linear units radial grid ( $n = 6$ ).

Making «n» of finite-difference equations (like 8) we receive a system of linear algebraic equations (SLAE) of 6-th order.

$$\begin{cases} 114,7u_1 - 65,556u_2 - 16,418u_3 + 0,212K^2 \cdot 10^{-6} = 0 \\ -65,556u_1 + 98,283u_2 - 65,556u_3 + 16,418u_4 + 2,212K^2 \cdot 10^{-6} = 0 \\ 16,418u_1 - 65,556u_2 + 98,283u_3 - 65,556u_4 + 16,418u_5 - 1,188K^2 \cdot 10^{-6} = 0 \\ 16,418u_2 - 65,556u_3 + 98,283u_4 - 65,556u_5 + 16,418u_6 - 1,188K^2 \cdot 10^{-6} = 0 \\ 16,418u_3 - 65,556u_4 + 114,70u_5 - 65,556u_6 - 1,188K^2 \cdot 10^{-6} = 0 \\ 32,838u_4 - 131,119u_5 + 98,283u_6 - 1,188K^2 \cdot 10^{-6} = 0 \end{cases} \quad (10)$$

Figure 6 shows a fragment of the radial grid.

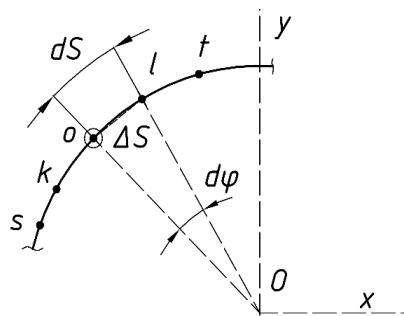


Figure 6 – Fragment of the radial grid

SLAE of 6th order (9) in matrix form can be written as:

$$(A - BK)\vec{u} = 0, \quad (11)$$

where A - a square matrix of order 6, composed of the coefficients of the appropriating units displacements  $u_1, u_2, \dots, u_6$ ;

B - a diagonal matrix of order 6, composed of the coefficients relating to the load parameter in units 1, 2, ... 6.

A nontrivial solution of the equation (11) when  $\vec{u} \neq 0$ , has the form:

$$D = A - B \cdot K = 0 \quad (12)$$

D - determinant of the 6-th order. Disclosing this determinant relatively in the parameter load "K" we get the characteristic equation of order 6, ie,

$$a_1 K^6 + a_2 K^5 + \dots + a_6 K^6 + b = 0 \quad (13)$$

Solving the characteristic equation (13) we get six of its roots (eigenvalues of the matrix «D»), each of which corresponds to its own vector of unit displacements (of 6 vectors) defining forms of stability loss of hingeless circular arches.

In practical tasks the actual value has a smaller value  $K_i$  ( $i=1, 2, \dots, 6$ ), i.e.  $K = K_{\min}$ , which corresponds to the critical load  $q_{kp}$  (expression 6), i.e.,

$$q_{kp} = \frac{EJ_{\min}(K_{\min}^2 - 1)}{R^2} \quad (14)$$

For the calculated arch scheme (See Figure 2) (calculated using the standard program "Matcad") received for SLAE (10) value:

$$K=K_{\min}=39,9832; \quad (15)$$

Then, by (14) the critical load equals

$$q_{kp} = \frac{EJ_{\min}(39,9832^2 - 1)}{0,06^2} = 443793,38 EJ_{\min},$$

i.e.  $q_{kp} = 443793,38 EJ_{\min}$  (kH/m).

The first form of the arch of loss stability (or values  $K_{\min}=39,9832$ ) is shown in Figure 7.

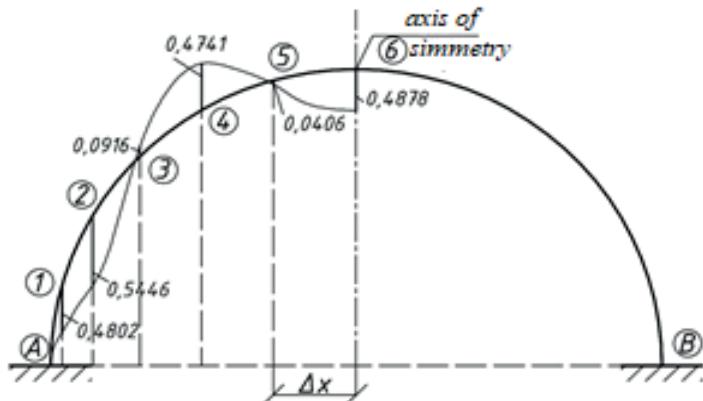


Figure 7 - The form of loss stability of hingeless arch

**Discussion.** Complex stress state that occurs when cutting different materials by rotating circular saw blades, in this research, it is modeled by the rod model in the form of a hingeless circular arch, loaded by radial and tangential loads. In the study of the reliability of such circular saw blades along with the issues of their strength are more important and the problem of stability of the Euler sense. Applied in the research the differential equations (5,7) of curved axis of the circular bar is adequately reflects the relationship between external influences and internal forces and displacements. The greatest bending moments are concentrated in the left half an arch in the lock area of an arch (Figure 3). The longitudinal force (Figure 5) acquires the highest values in the right half an arch and have different symbolic value (on the diagram - three half-wave).

The finite difference method, applied for the stability study provides sufficient engineering accuracy (estimated at six units - taking into account the symmetry of the arch).

The value of the critical load ( $q_{kp}$ ) provides stability to the circular saw blade

solid stability supplies is more than one. Form of loss stability (Figure 7) has a complex multi-wavelength character in view of the nature of a complex scheme of loading blade (Figure 2).

**Conclusions.** It is showed the effectiveness of the use of the finite difference method for the calculation of the state of stability of the saw blade, using the rod model calculation in the form of a hingeless circular arch for half circular saw blade pierced into the body of the material being cut.

The form of the loss of stability in a complex scheme of loading (see. Fig. 2) has a “multiwave” character (see. Fig. 7).

The proposed methodology of calculation on stability can be applied to other calculated arches schemes (with other conditions equations arch basing axle, loading schemes).

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